

WEC-Sim Technical Training Course

for users and developers

9/8/2023

PRESENTED BY

Jeff Grasberger

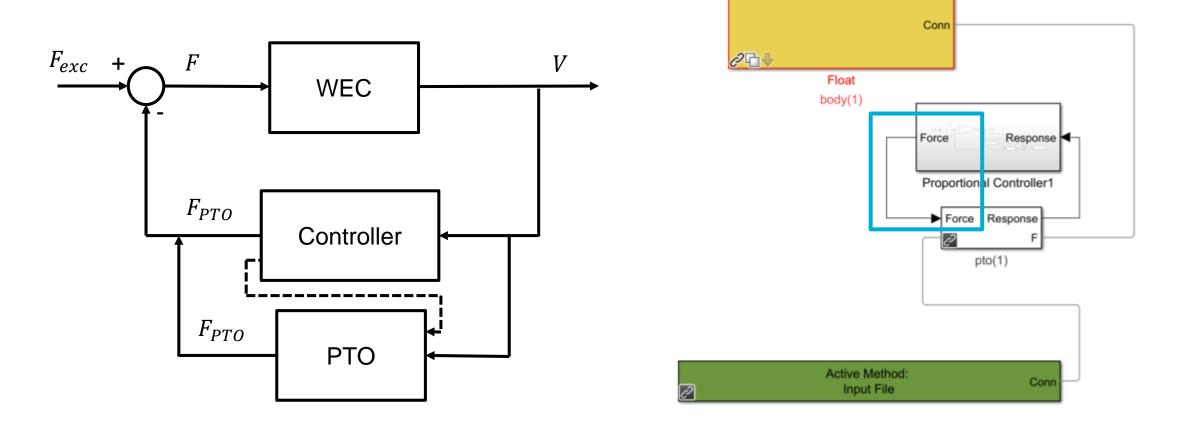


WEC-Sim Controls

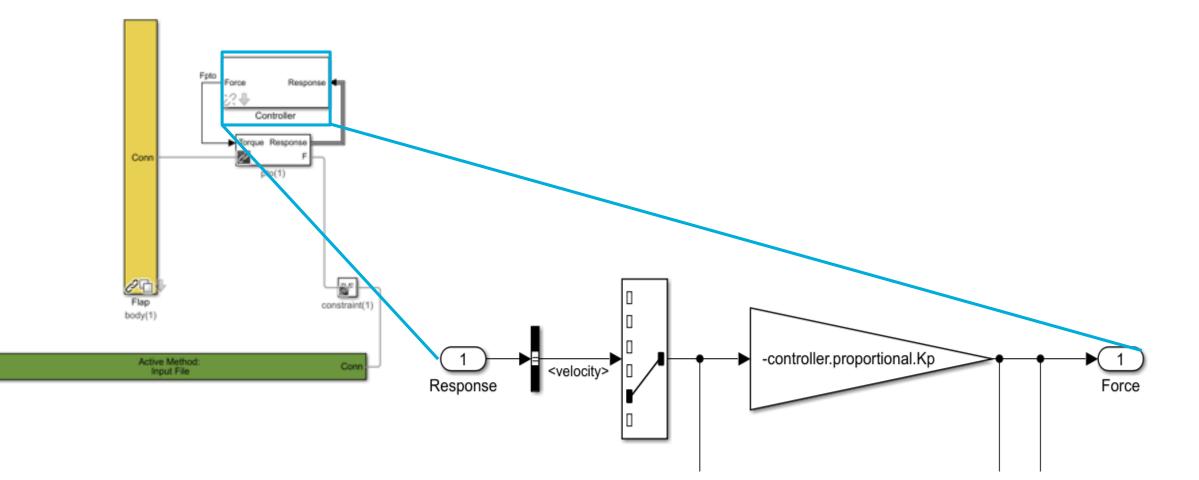
2

³ WEC Control Background – PTO Force

WEC controls prescribes PTO force: $u=F_{PTO}$



4 WEC-Sim Control Implementation

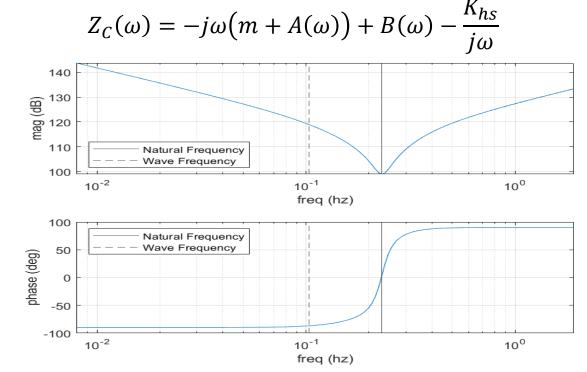


5 WEC Control Background – Complex Conjugate Impedance Matching

- Optimal control maximizes harvested power
- Power transferred to the WEC can be maximized through complex conjugate impedance matching
 - WEC Intrinsic Impedance:

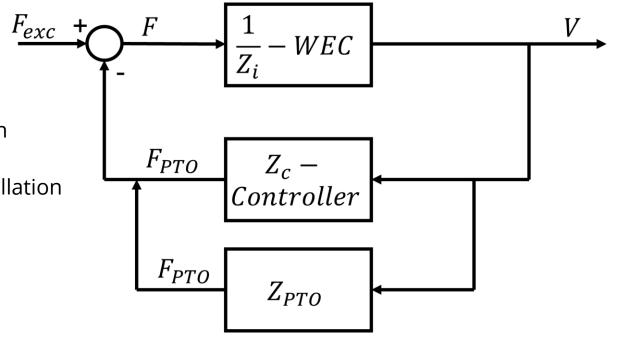
$$Z_{i}(\omega) = j\omega(m + A(\omega)) + B(\omega) + \frac{K_{hs}}{j\omega}$$

Complex Conjugate Controller Impedance:



6 WEC Control Types

- **Passive** (proportional: P) Damping Force
- Reactive (proportional-integral: PI) Damping and Spring Force
- Phase Control:
 - **Latching** Locking device for part of oscillation
 - **Declutching** Releasing device for part of oscillation
- Model Predictive Control Predicts and
 optimizes dynamics for maximum power



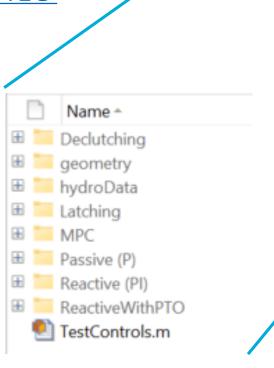
7 VEC Control Examples

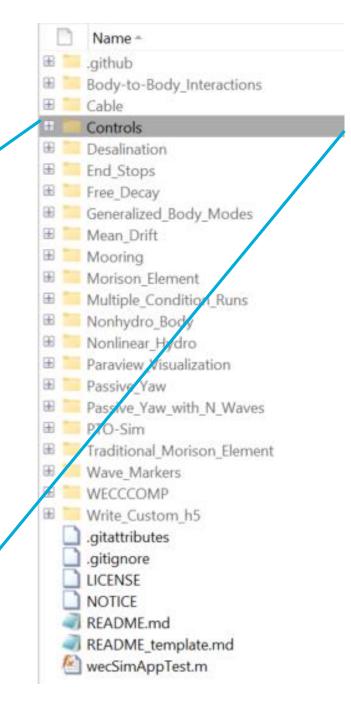
• WEC control examples are available on the WEC-

Sim Applications repository:

https://github.com/WEC-Sim/WEC-

Sim_Applications





WEC Control – Passive (P) 8

Applied PTO force is proportional to velocity: •

 $F_{PTO} = K_p \dot{X}$

- Damping force •
- •

• Theoretical optimal gain:

$$K_{p,opt} = \sqrt{B(\omega)^2 + \left(\frac{K_{hs}}{\omega} - \omega(m + A(\omega))\right)^2}$$
WEC motion
WEC motion

Requires no input power •

 $K_p - PTO$

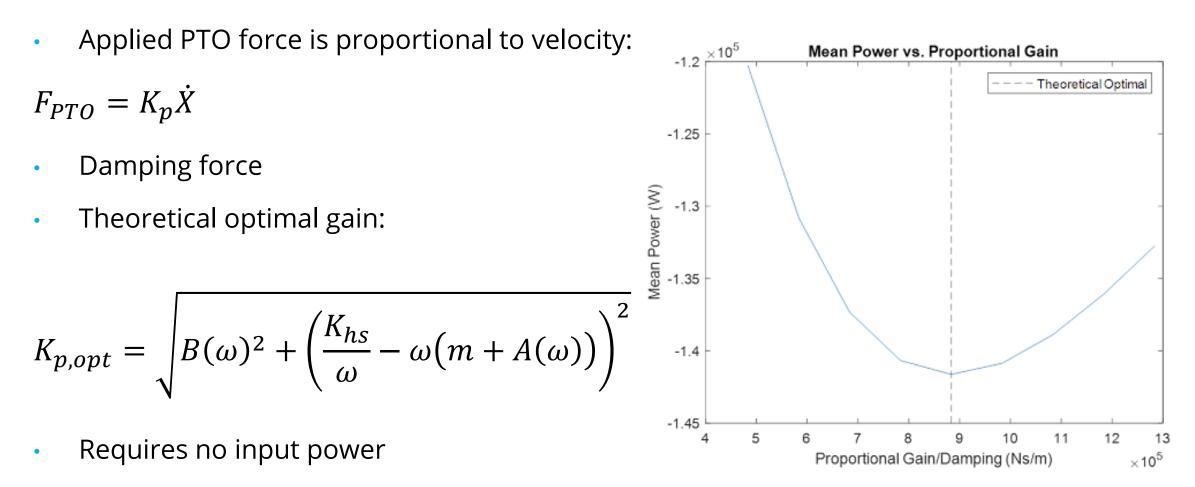
Damping

Excitation and

Buoyancy

Forces

9 WEC Control – Passive (P)



Note: negative power is power harvested

10 WEC Control – Reactive (PI)

• Applied PTO force is proportional to position and velocity:

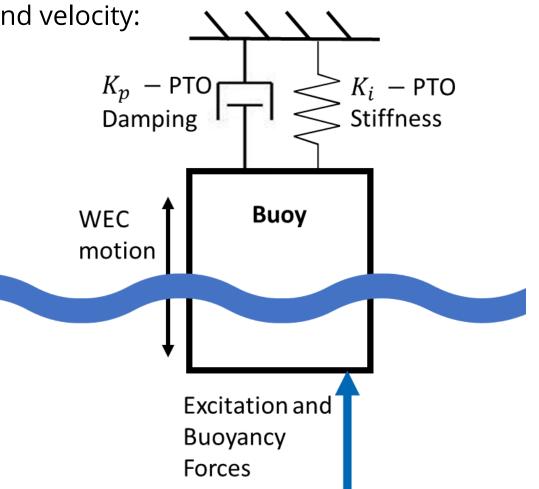
 $F_{PTO} = K_p \dot{X} + K_i X$

- Damping and spring force
- Theoretical optimal gains:

 $K_{p,opt} = B(\omega)$

 $K_{i,opt} = (m + A(\omega))\omega^2 - K_{hs}$

Reactive component requires input power



11 WEC Control – Reactive (PI)

• Applied PTO force is proportional to position and velocity:

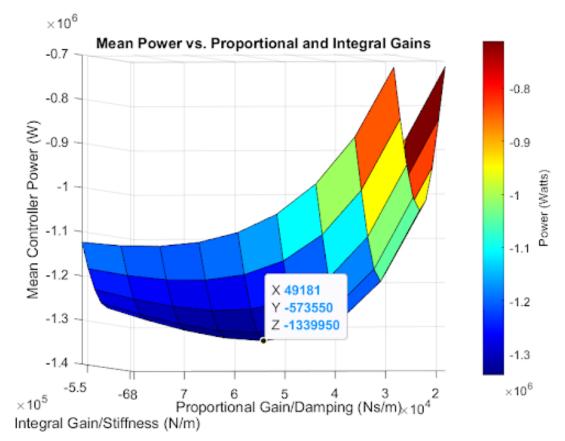
 $F_{PTO} = K_p \dot{X} + K_i X$

- Damping and spring force
- Theoretical optimal gains:

 $K_{p,opt}=B(\omega)$

 $K_{i,opt} = \left(m + A(\omega)\right)\omega^2 - K_{hs}$

• Reactive component requires input power Note: negative power is power harvested



12 WEC Control – Latching

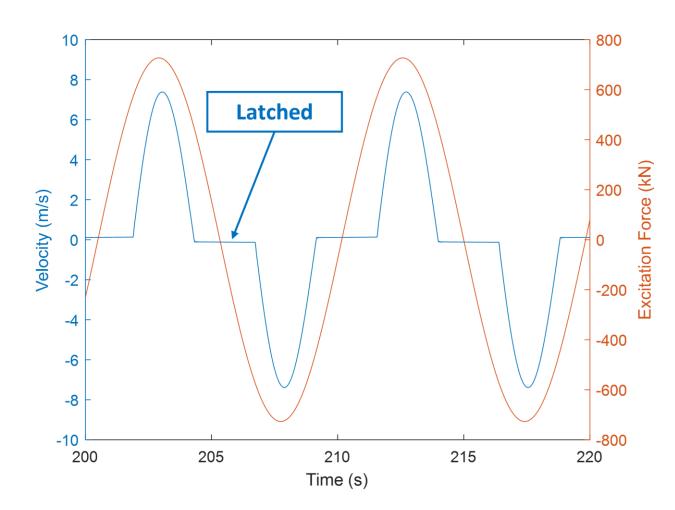
- Passive controller + locking device
- Braking force:

 $G = 80(m + A(\omega))$

• Theoretical optimal latch time:

$$t_{latch} = \frac{1}{2} \left(T_{wave} - T_{nat} \right)$$

• No input power required



13 WEC Control – Latching

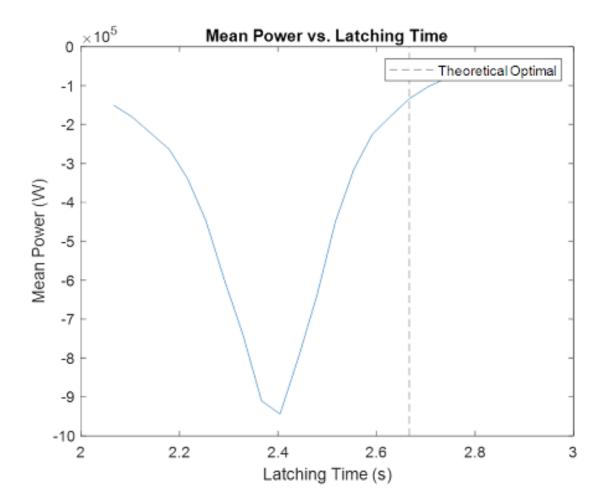
- Passive controller + locking device
- Braking force:

 $G = 80(m + A(\omega))$

• Theoretical optimal latch time:

$$t_{latch} = \frac{1}{2} \left(T_{wave} - T_{nat} \right)$$

No input power required
 Note: negative power is power harvested

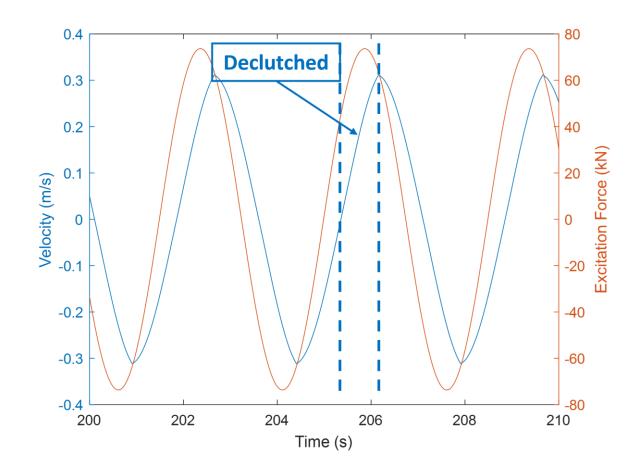


14 WEC Control – Declutching

- Passive controller + releasing device
- Allow device to move without damping force for part of oscillation
- Theoretical optimal declutch time:

$$t_{latch} = \frac{1}{2} \left(T_{nat} - T_{wave} \right)$$

• No input power required

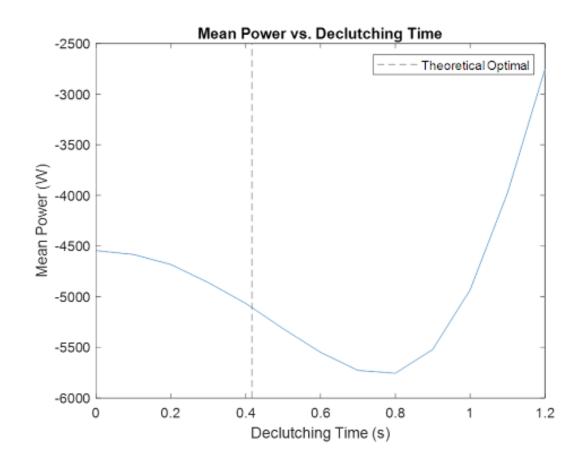


15 WEC Control – Declutching

- Passive controller + releasing device
- Allow device to move without damping force for part of oscillation
- Theoretical optimal declutch time:

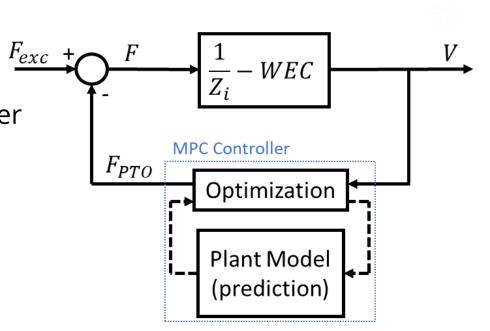
$$t_{latch} = \frac{1}{2} \left(T_{nat} - T_{wave} \right)$$

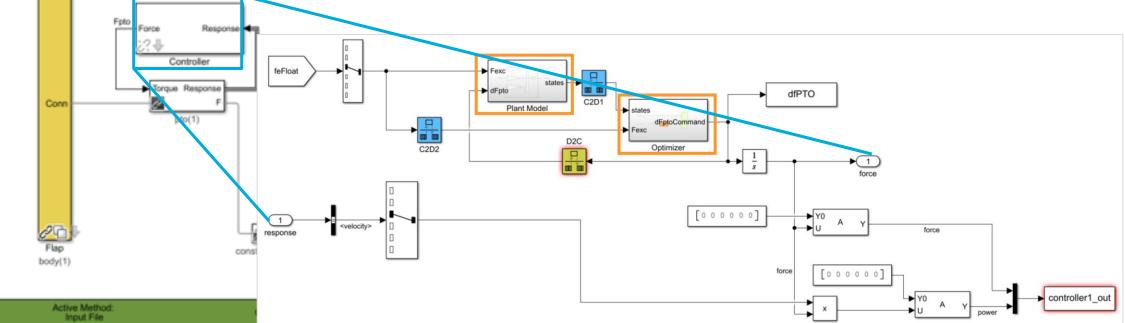
• No input power required Note: negative power is power harvested



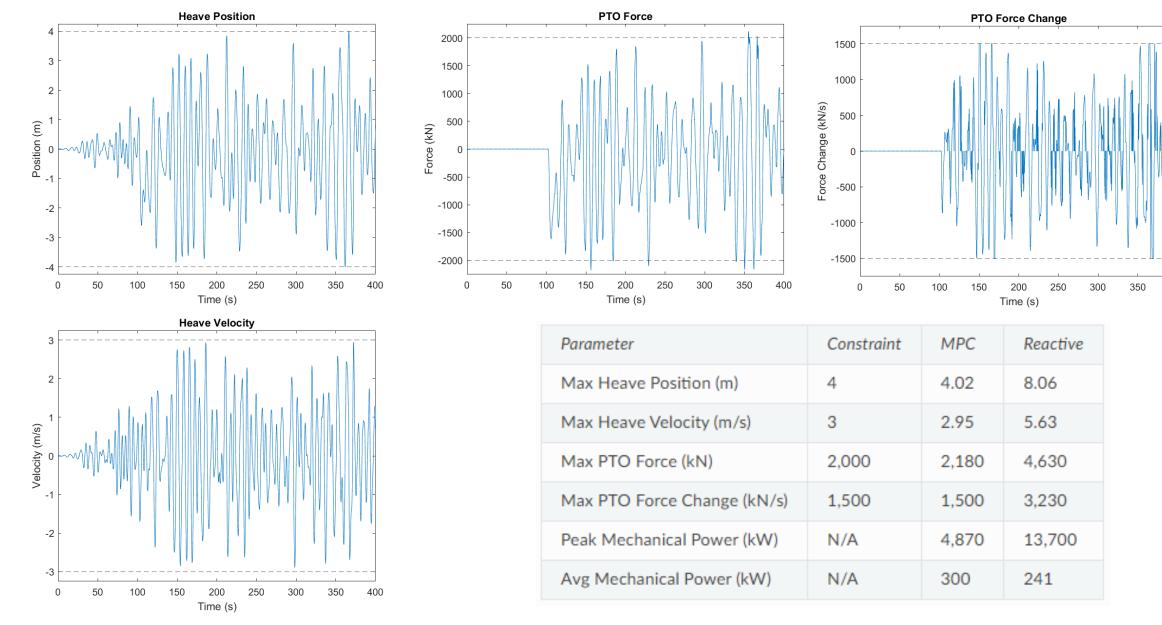
16 WEC Control – Model Predictive Control (MPC)

- Predicts and optimizes dynamics for maximum power
- State space plant model used to predict dynamics
- Quadprog() used to optimize for maximum power
- Can apply time-domain constraints





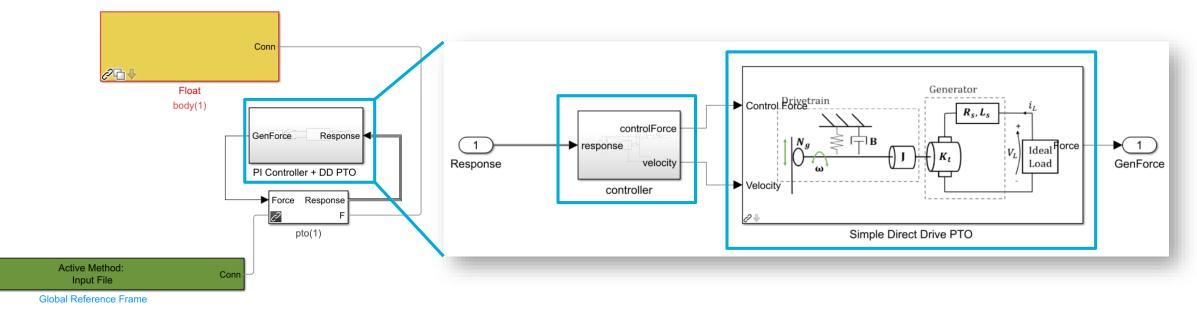
¹⁷ WEC Control – Model Predictive Control (MPC)



400

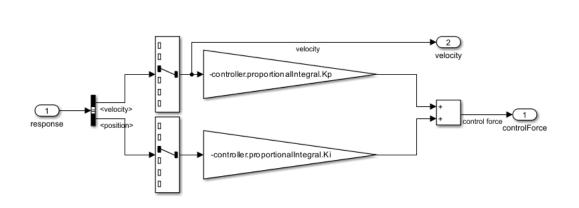
18 WEC Control – Integration with PTO-Sim

- Effective WEC control NEEDS to be linked with a power take-off system to calculate electrical power
- Optimal mechanical power ≠ optimal electrical power
- Complex conjugate control often leads to conditions that are inefficient for PTO power extraction
- Controller determines desired force which is fed into PTO to apply force and calculate electrical power



¹⁹ WEC Control – Integration with PTO-Sim

+

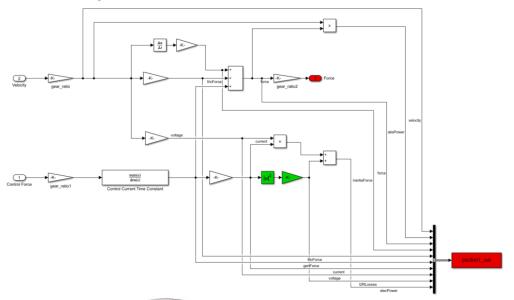


Reactive controller

PTO Parameters

Parameter	Value	Unit		
Torque Constant (Kt)	7.186	Nm/A		
Gear Ratio (N)	100			
Inertia (J)	2	kg/m^2		
Mechanical Shaft Damping (B)	1	Nms		
Resistance (R)	0.483	Ω		
Inductance (L)	5.223	mH		

simplified direct drive PTO





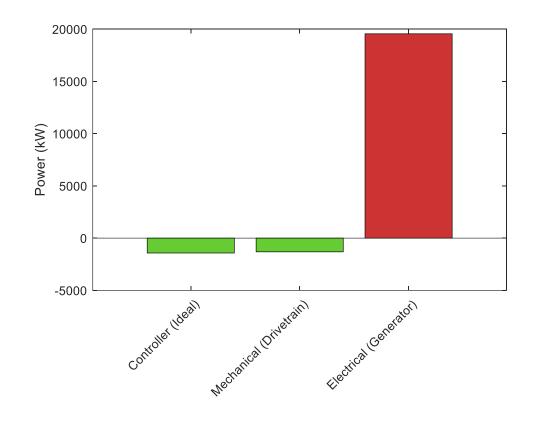
Allied Motion Megaflux™ Frameless Direct Drive Torque Motors

²⁰ WEC Control – Integration with PTO-Sim

- Maximization of mechanical power (aka complex conjugate control) requires significant input electrical power
- Kp = 49,200 N/m, Ki = -573,000 Ns/m

Note: negative power is power harvested

Component	Power (kW)					
Controller (Ideal)	-1,400					
Mechanical (Drivetrain)	-1,300					
Inertia	0					
Damping	300					
Generator Mechanical	-1,600					
Electrical (Generator)	19,600					
Current*Voltage	-1,600					
Electrical Power Loss (I^2*R)	21,200					

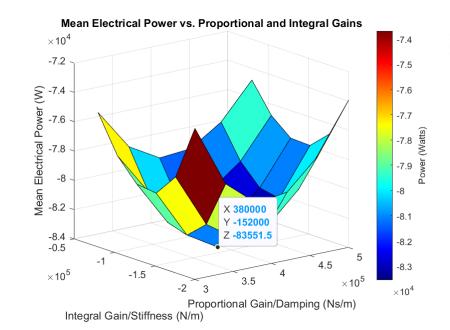


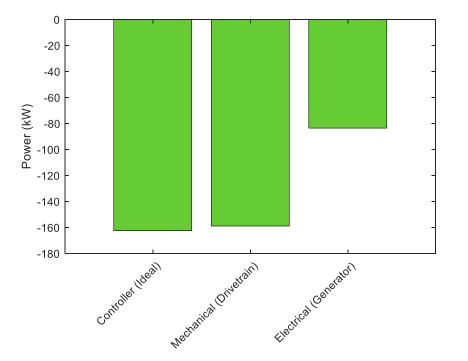
²¹ WEC Control – Integration with PTO-Sim

- Larger proportional (Kp) and smaller integral (Ki) gains support optimal electrical power
- Kp = 380,000 Ns/m, Ki = -152,000 N/m

Note: negative power is power harvested

Component	Power (kW)				
Controller (Ideal)	-162				
Mechanical (Drivetrain)	-159				
Inertia	0				
Damping	4				
Generator Mechanical	-163				
Electrical (Generator)	-84				
Current*Voltage	-163				
Electrical Power Loss (I^2*R)	80				





📣 MATLAB R2022b																			_		\times
HOME	PLOTS	APPS		_						_							1 9 0	🛱 🕐 💿 Search	Documentation	🎗 🤦	Jeff 🔻
New New Script Live Script	New Ope	Find File	Import	t Clean	Variable	orkspace	Favorites	Analyze Code Code Code Code Code Code Code Code	Simulink	Layout	 Preferences Set Path Parallel ENVIRONMENT 	Add-Ons	Help	Community Request Support Learn MATLAB RESOURCES							Ā
🧇 🔶 🖬 💭 📁	C: User	s 🕨 jtgrasb 🕨	Document	ts 🕨 Gi	tHub 🕨 WEC	-Sim_Applicat	ions 🕨														- P
Current Folder					۲	Command	Window														۲
Name +					Git	<i>fx</i> : >>															
Generalized B Generalized B Generalized B Mean_Drift Mooring Morison_Elem Moltiple_Conn Nonhydro_Bo Nonlinear_Hyu Passive_Yaw Passive_Yaw Po-Sim Traditional_M Write_Custom gitiattributes gitignore UCENSE NOTICE README_tem wecSimAppTe Details	iody_Modes nent dition_Runs vdy alalization with_N_Wave orison_Elem s n_h5	15		Value												I					
1111.																					
								Q Sear	ch			.		I 🧿 🗖	8 🐢 🕫 9 🔸					2:24 8/29/20	
															· · · ·						

Thank you

For more information please visit the WEC-Sim website:

http://wec-sim.github.io/WEC-Sim

If you have questions on this presentation please reach out to any of the WEC-Sim Developers on GitHub:

https://github.com/WEC-Sim/WEC-Sim

Sandia National Laboratories is a multimission laboratory managed and operated by National Technology & Engineering Solutions of Sandia, LLC, a wholly owned subsidiary of Honeywell International Inc., for the U.S. Department of Energy's National Nuclear Security Administration under contract DE-NA0003525.

This work was authored in part by the National Renewable Energy Laboratory, operated by Alliance for Sustainable Energy, LLC, for the U.S. Department of Energy (DOE) under Contract No. DE-AC36-08GO28308.

Funding provided by the U.S. Department of Energy Office of Energy Efficiency and Renewable Energy Water Power Technologies Office. The views expressed in the article do not necessarily represent the views of the DOE or the U.S. Government. The U.S. Government retains and the publisher, by accepting the article for publication, acknowledges that the U.S. Government retains a nonexclusive, paid-up, irrevocable, worldwide license to publish or reproduce the published form of this work, or allow others to do so, for U.S. Government purposes.



##